

# **Simplifying Kinematic Models through Geometric Constraints**

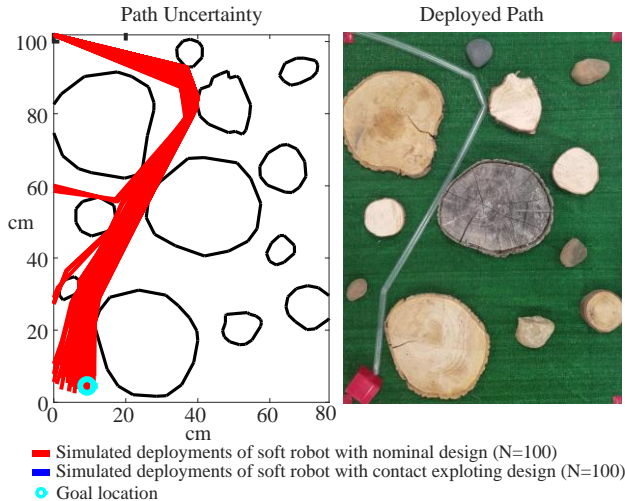
**Dr. Laura H. Blumenschein**  
Department of Mechanical Engineering  
Purdue University

## Design through geometric constraints and simplified kinematic models

- High link between **morphology** and **behavior** of soft robots
- Modeling can be a useful design tool, if models are simple enough
- Geometric constraints create simple building blocks that can be repeated to create complex behaviors
- Combination of simplified modeling and geometric constraints yields design principles for creating complex and useful kinematics from compliant systems

# Applying geometric constraints to simplify kinematic models

## Obstacle interaction to decrease uncertainty



Greer, et al (2020). "Robust navigation of a soft growing robot by exploiting contact with the environment," *IJRR*.

## Geometric models of general actuation



Blumenschein, et al (2020). "Geometric Solutions for General Actuator Routing on Inflated-Beam Soft Growing Robots," *arXiv preprint arXiv:2006.06117*.

## Design of soft delta mechanisms



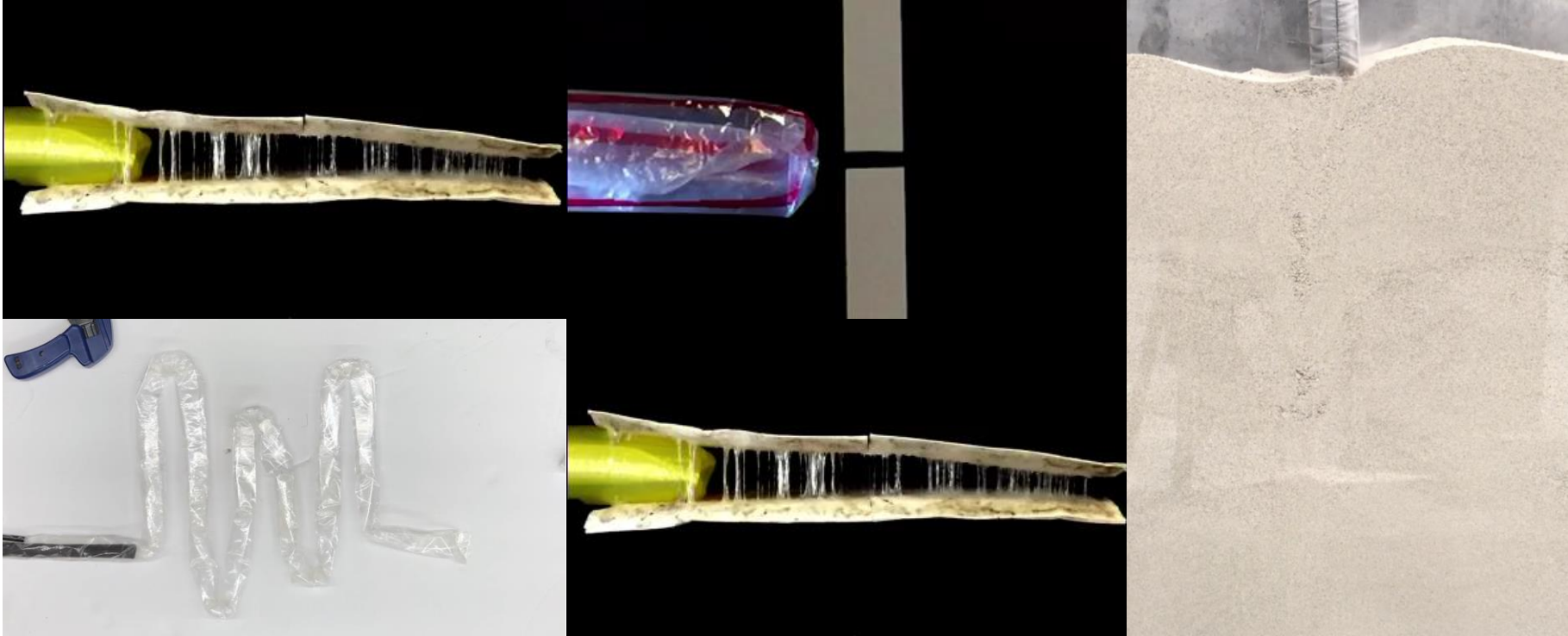
Blumenschein, et al (2019) "Generalized Delta Mechanisms from Soft Actuators," RoboSoft.

# Introduction

## Pneumatic Tip-Extending Soft Robot



## Growing Affects Environmental Interactions



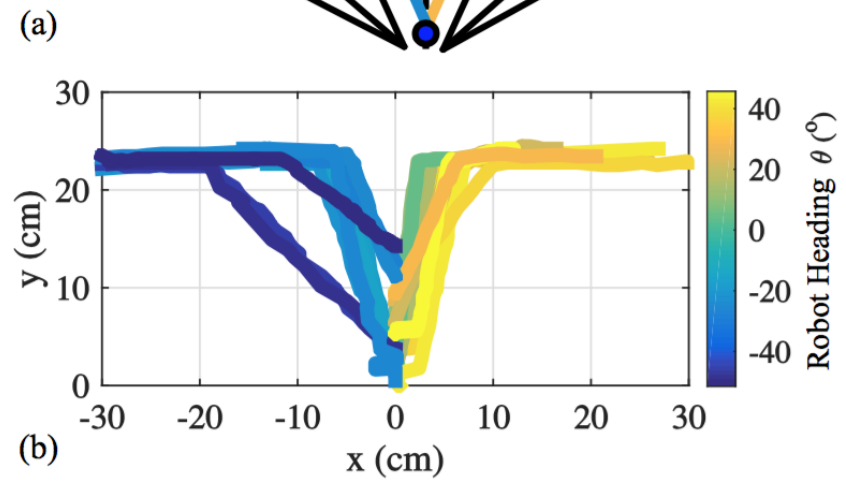
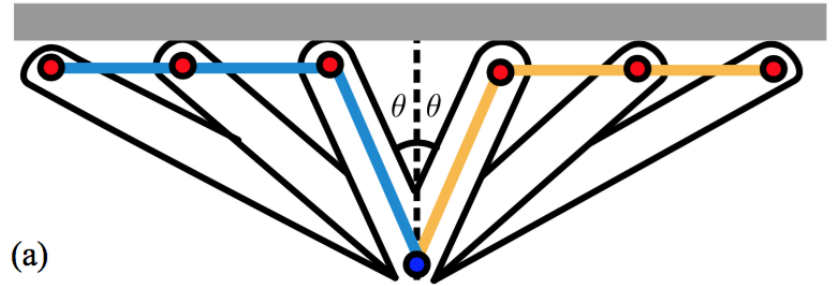
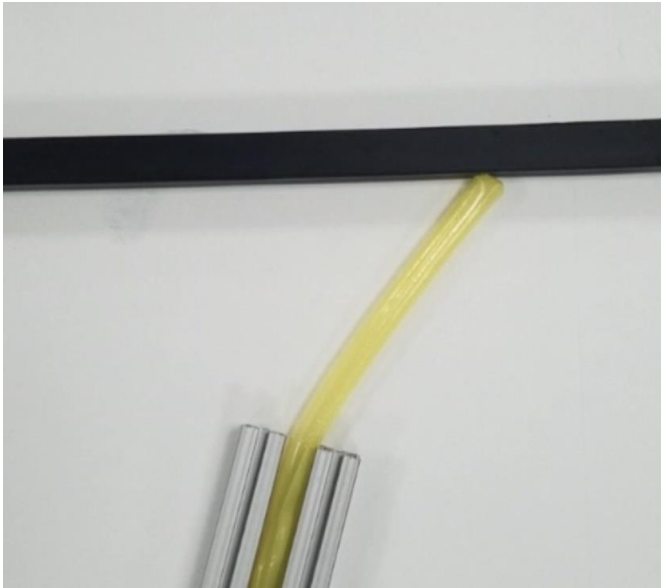
Question: How do we harness environment interactions to improve navigation?

## Useful Obstacle Interaction Behavior



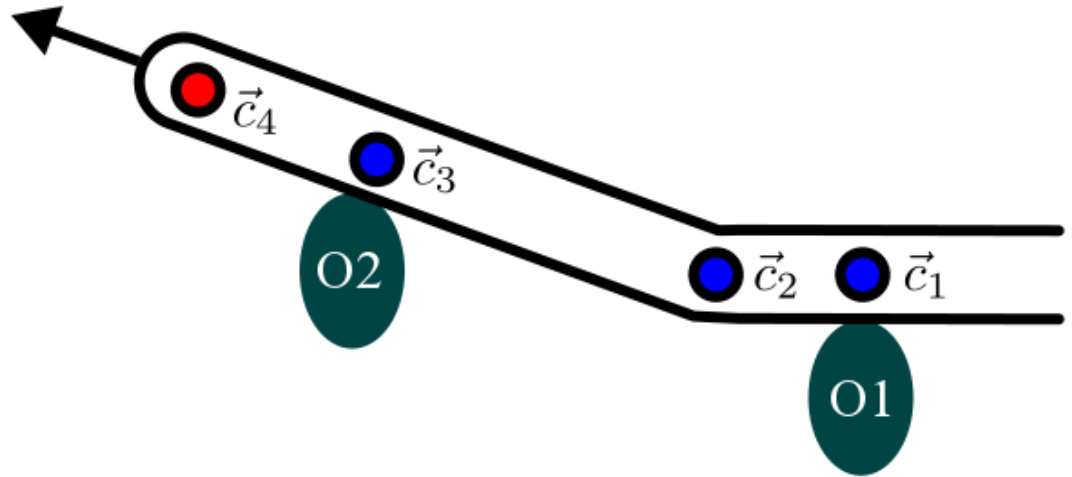
Environment passively guides the robot

# Varying the Initial Contact Angle



## Building an Obstacle-Aided Navigation Model: Robot State

- Robot state = pivot points
- Pivot points (two types):
  - Obstacle contact
  - Pre-made turn
- Obstacle contacts added as encountered





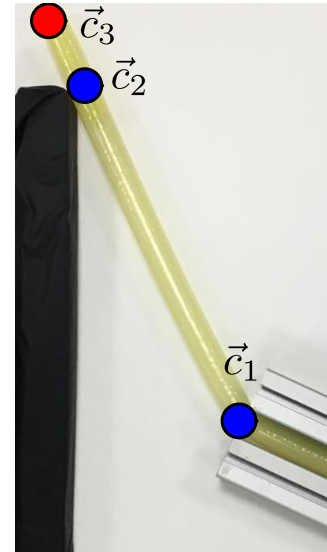
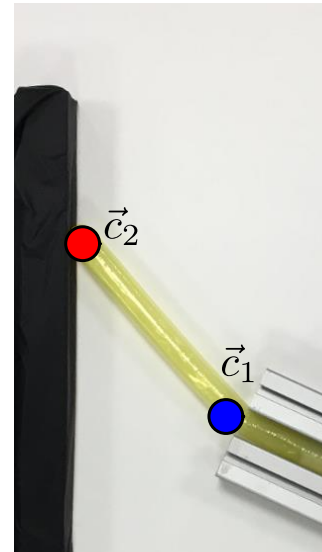
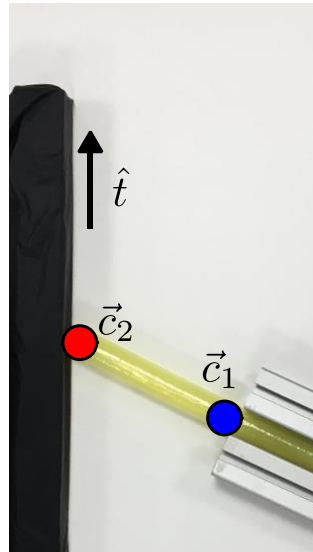
# Building an Obstacle-Aided Navigation Model: Kinematics

Free-Growth Differential Kinematics:

$$\dot{\vec{c}}_n = u \frac{1}{\|\vec{c}_n - \vec{c}_{n-1}\|} (\vec{c}_n - \vec{c}_{n-1})$$

Obstacle Contact Differential Kinematics:

$$\dot{\vec{c}}_n = u \frac{\|\vec{c}_n - \vec{c}_{n-1}\|}{\hat{t} \cdot (\vec{c}_n - \vec{c}_{n-1})} \hat{t}$$



$u \left( \frac{m}{s} \right)$  is controlled growth rate

## Model Validation: Navigation by Obstacles Only

# Obstacle-Aided Navigation of a Soft Growing Robot

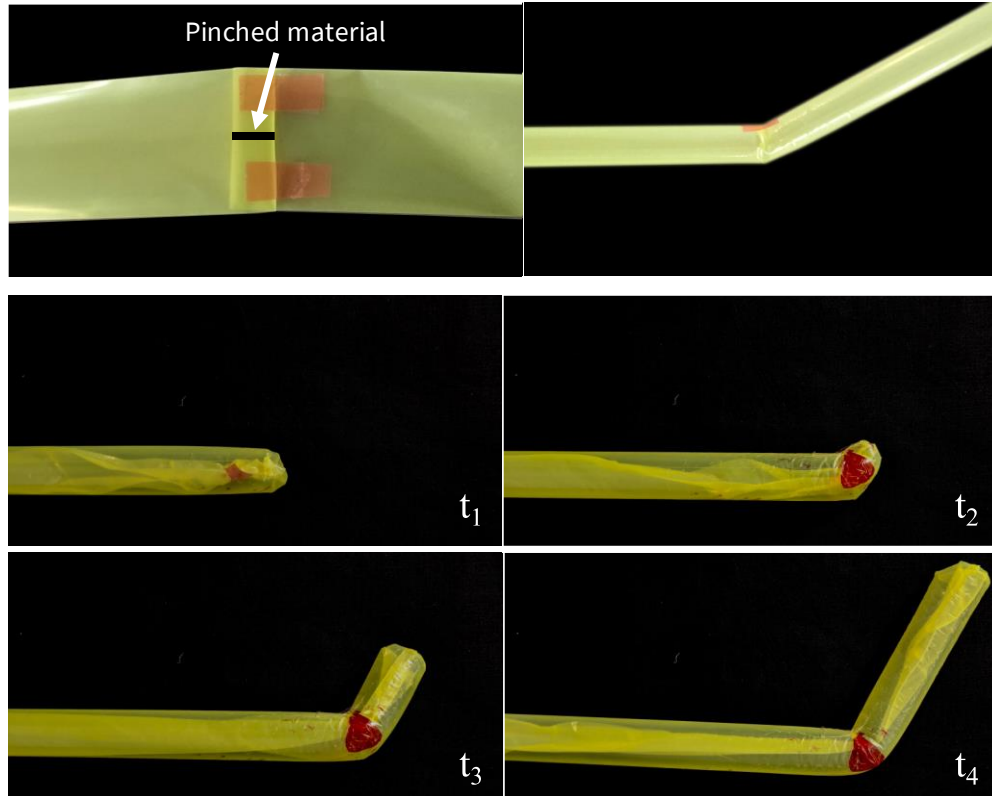
Joseph D. Greer<sup>1</sup>, Laura H. Blumenschein<sup>1</sup>,  
Allison M. Okamura<sup>1</sup>, and Elliot W. Hawkes<sup>2</sup>

<sup>1</sup> Stanford University

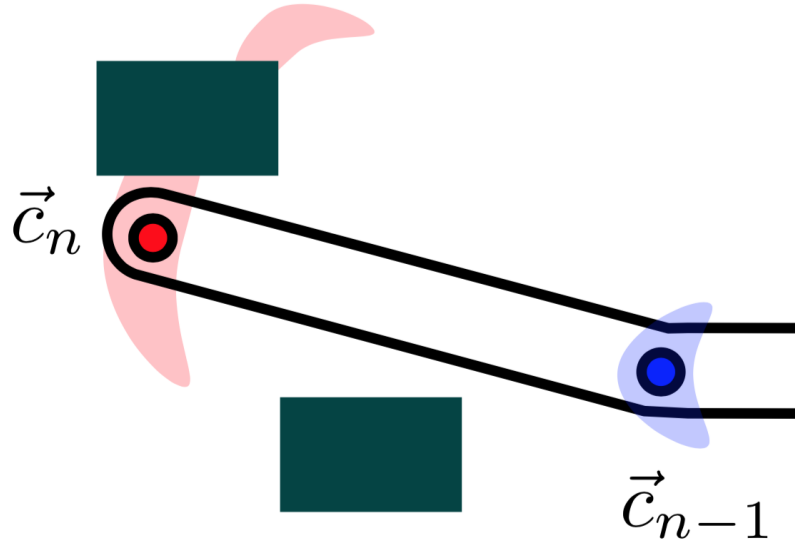
<sup>2</sup> University of California, Santa Barbara

# Adding in Steering

Uniformly shorten one side



# Planning Robot Paths to Intelligently Use Obstacle Contacts



Nominal design:  $(\underline{l}_1, \underline{\theta}_1, \dots, \underline{l}_m, \underline{\theta}_m)$

Manufacturing Error ↓

Built design:  $(\underline{\hat{l}}_1, \underline{\hat{\theta}}_1, \dots, \underline{\hat{l}}_m, \underline{\hat{\theta}}_m)$

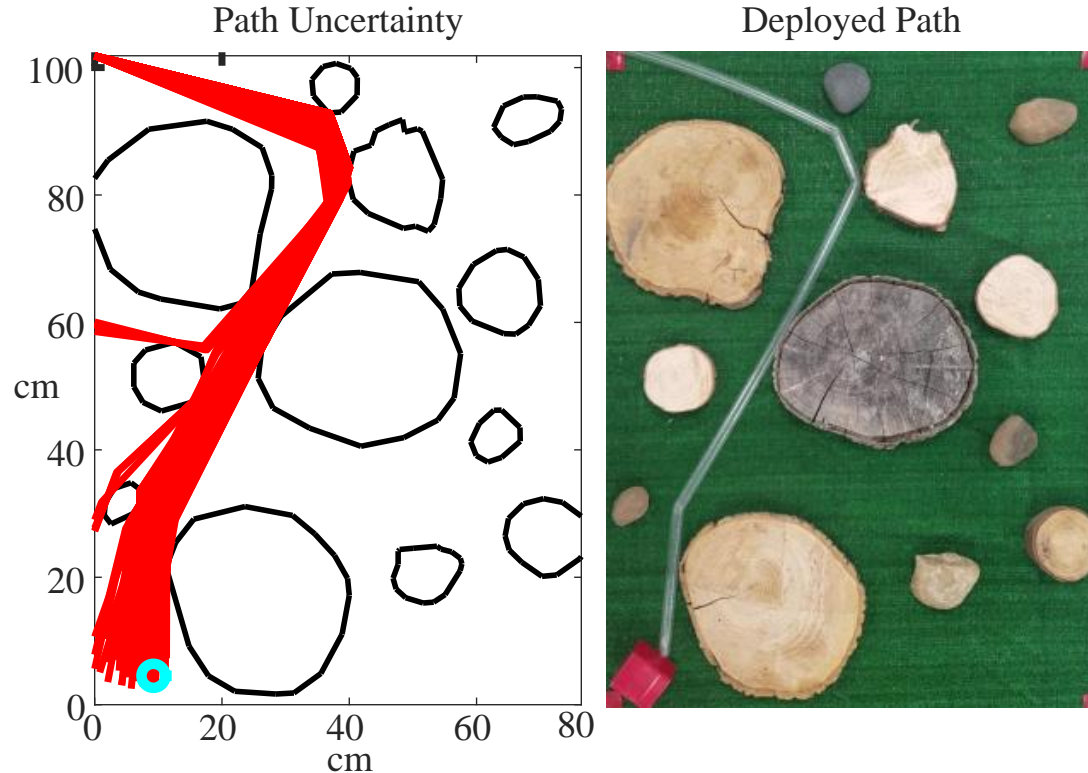
## Planning Objective:

Find nominal design with highest expectation of reaching desired target given obstacle interactions

# Planning In a Cluttered Environment



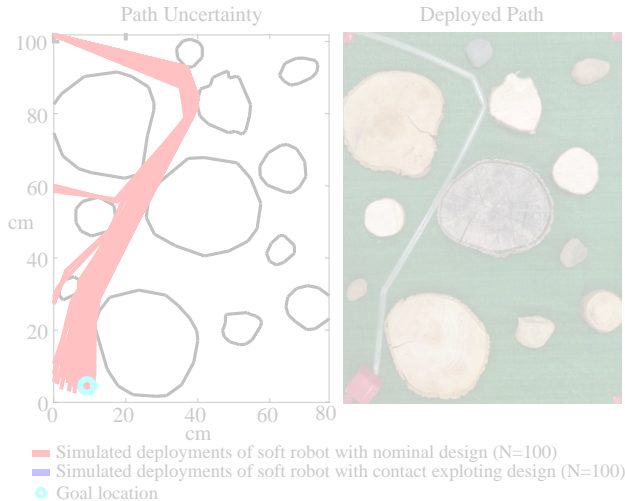
# Planning In a Cluttered Environment



- Simulated deployments of soft robot with nominal design (N=100)
- Simulated deployments of soft robot with contact exploring design (N=100)
- Goal location

# Applying geometric constraints to simplify kinematic models

## Obstacle interaction to decrease uncertainty



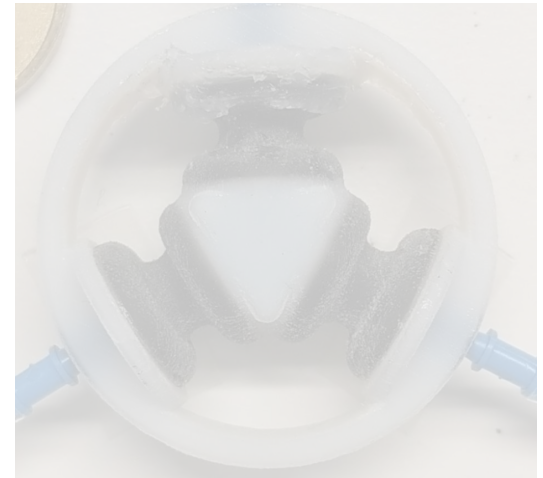
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## Geometric models of general actuation



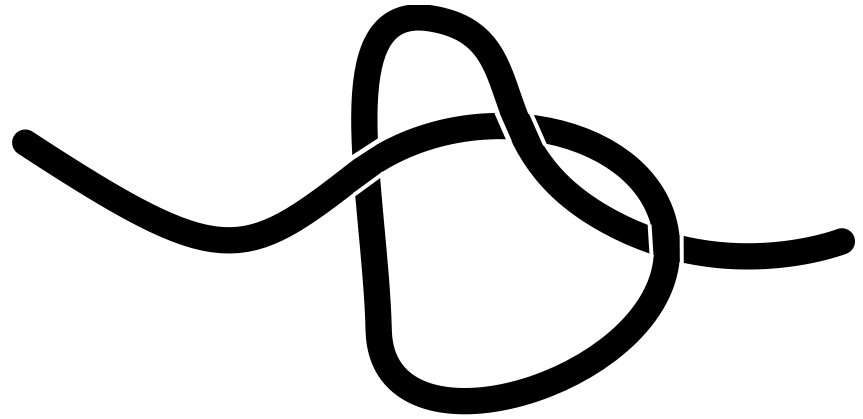
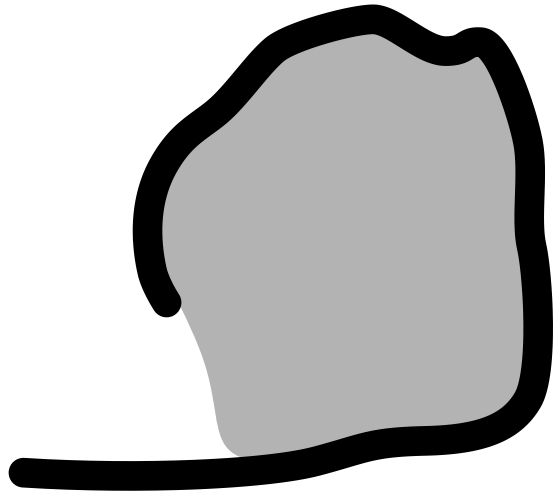
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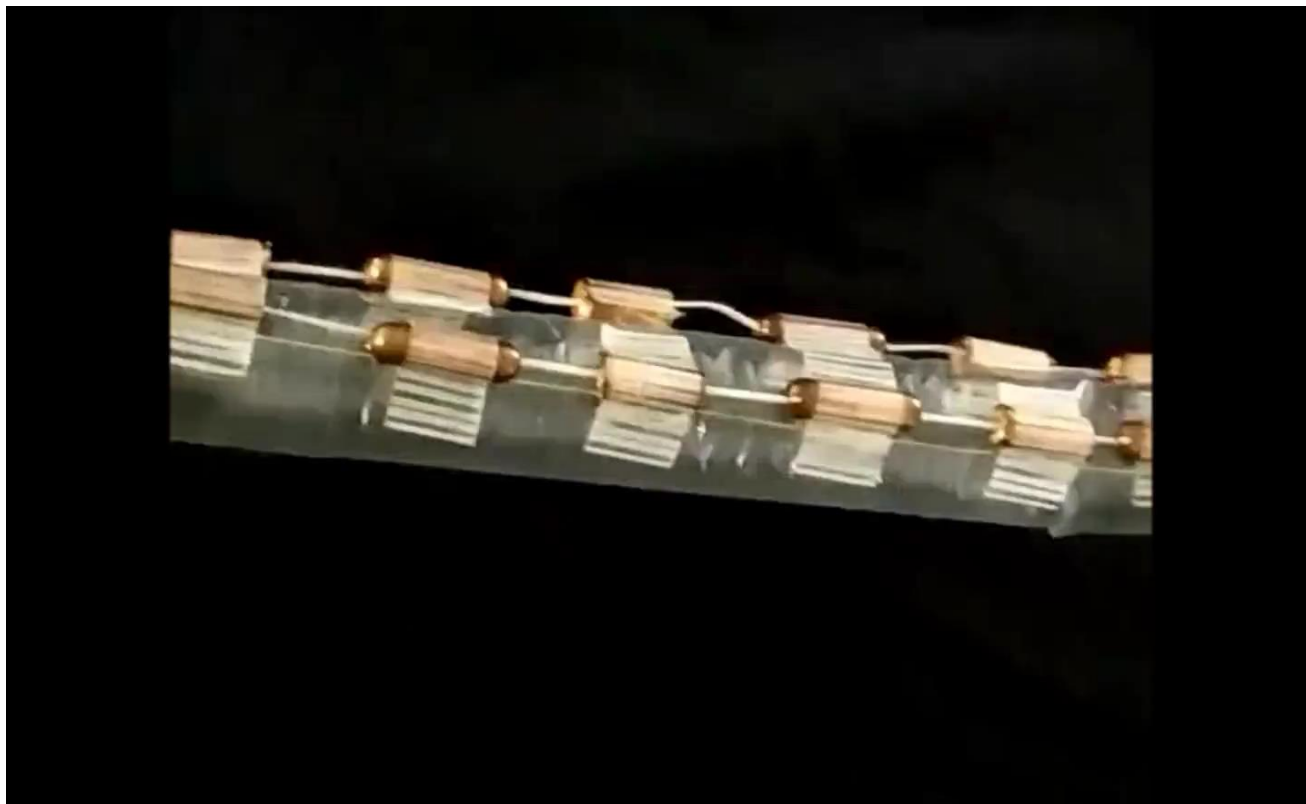
How do we achieve a desired shape of a growing robot through active actuation?





# Designing Active Steering

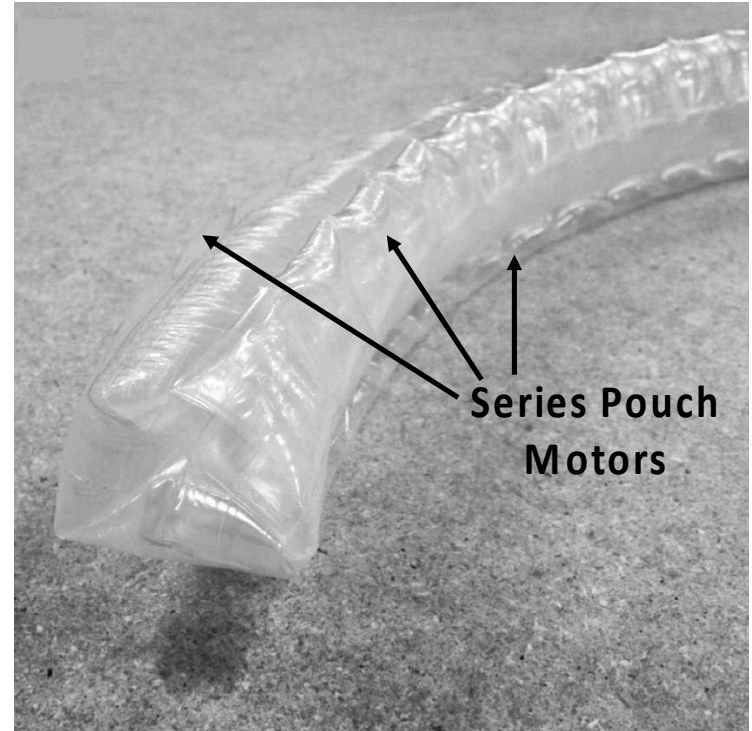
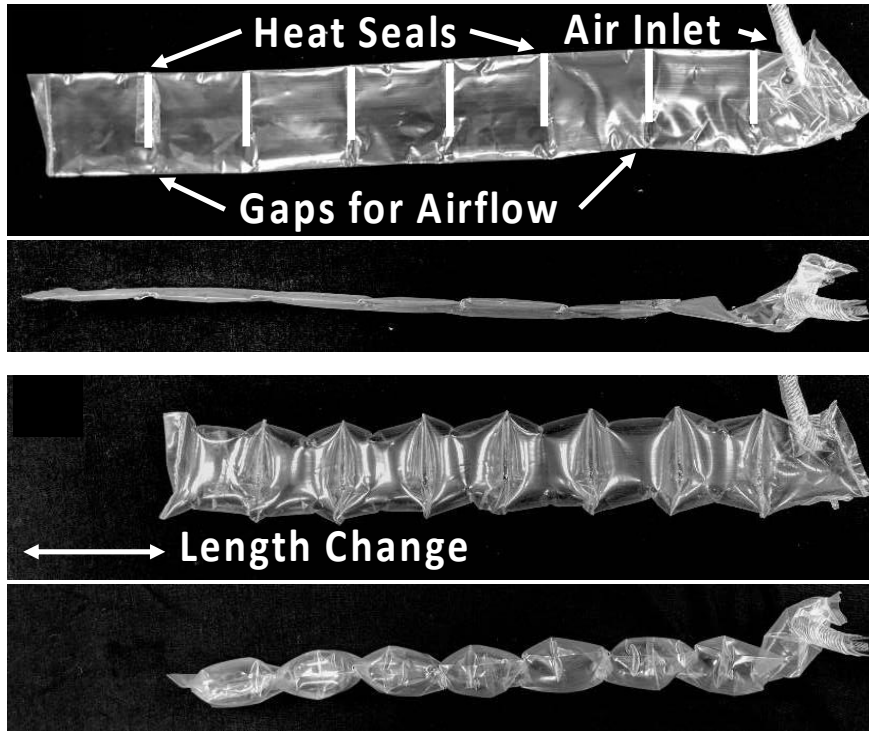
## Tendon Actuation



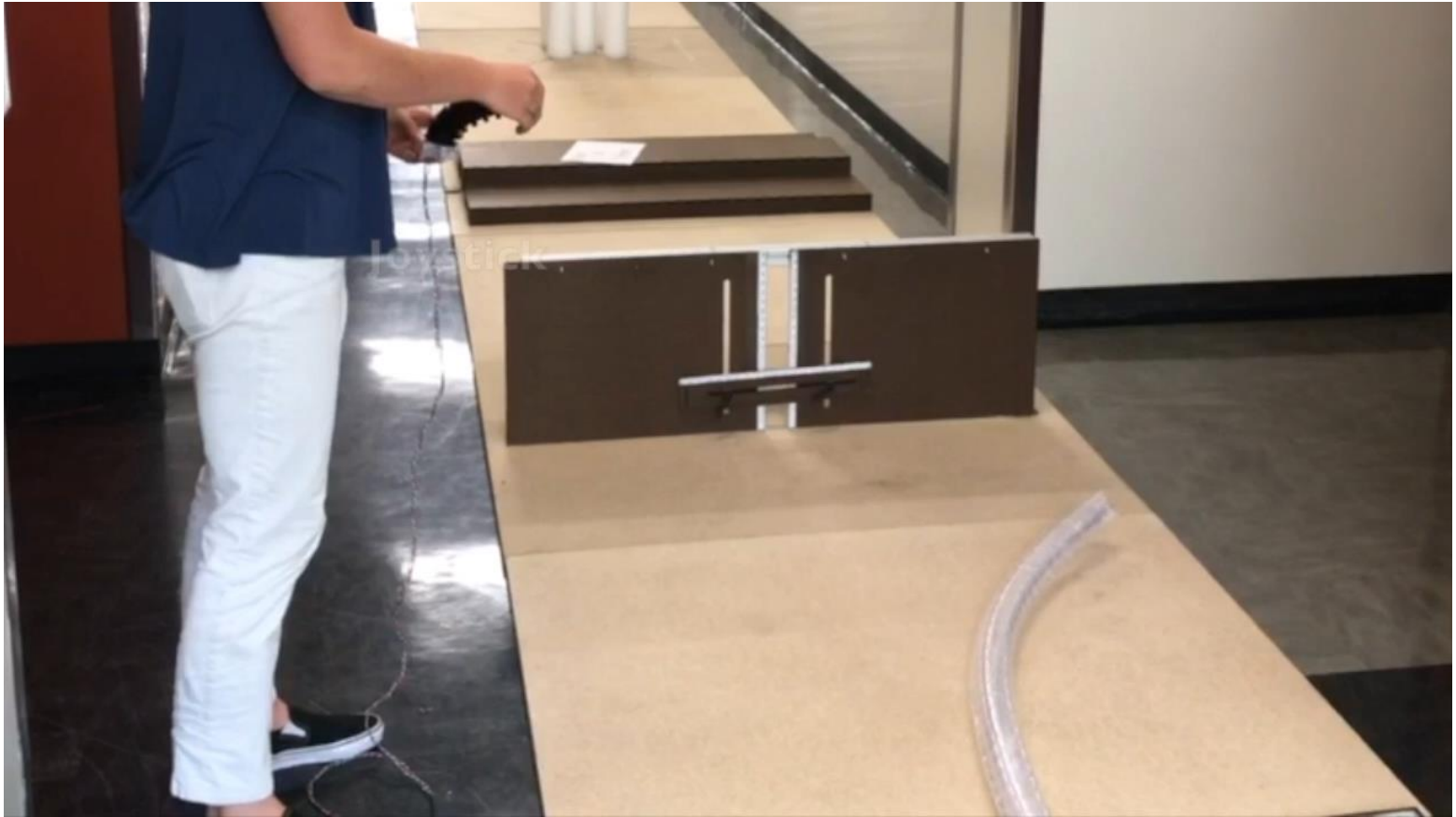
L. Gan, **L. H. Blumenschein**, Z. Huang, A. M. Okamura, E. W. Hawkes, and J. Fan (Accepted) 3D Electromagnetic Reconfiguration Enabled by Soft Continuum Robots. IEEE Robotics and Automation Letters, 2020.

# Designing Active Steering

## Pneumatic Actuation

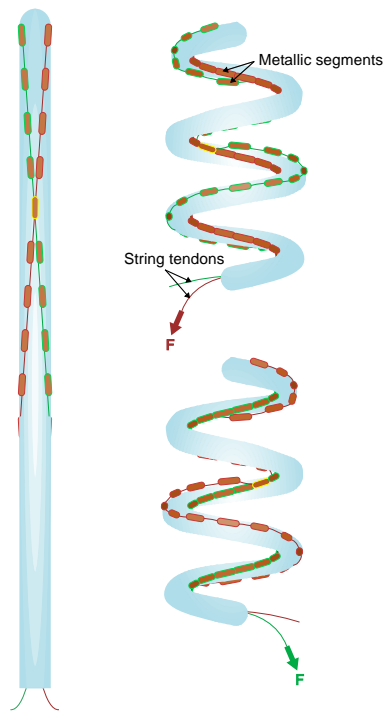
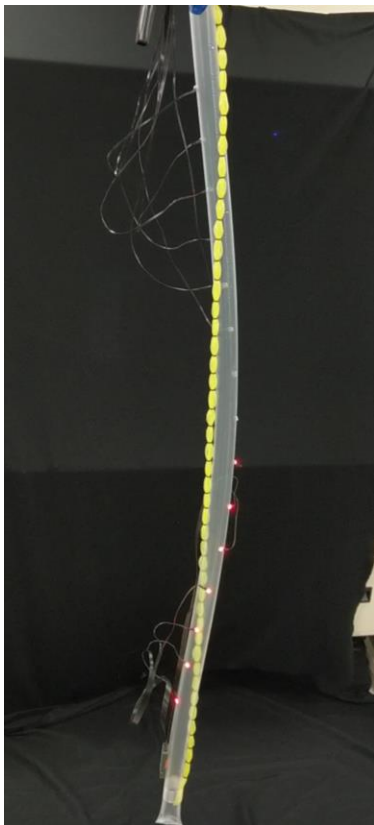


## Designing Active Steering



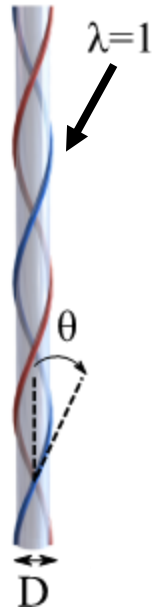
J. D. Greer, T. K. Morimoto, A. M. Okamura, and E. W. Hawkes. Series Pneumatic Artificial Muscles (sPAMs) and Application to a Soft Continuum Robot. ICRA 2017. A Soft, Steerable Continuum Robot that Grows via Tip Extension. *Soft Robotics*, in press.

# Creating More Complex Shapes

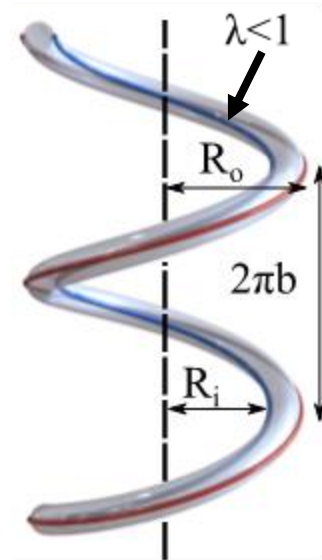


# General Actuator Kinematics

## Uniform Actuation



Actuate blue path

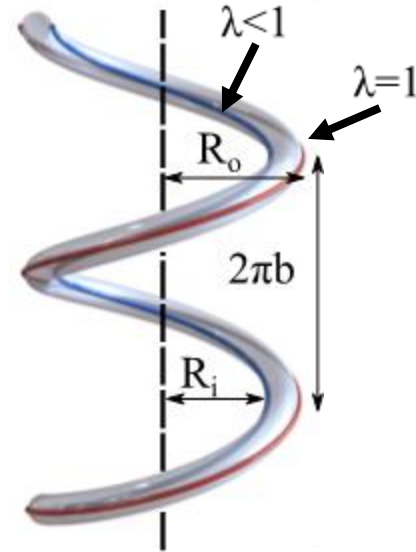


# General Actuator Kinematics

## Geometric Constraint: Path Length

Inner helix arc length is shortened relative to the outer helix:

$$\lambda = \frac{\sqrt{b^2 + R_i^2}}{\sqrt{b^2 + R_o^2}}$$



# General Actuator Kinematics

## Geometric Constraint: Cross-Sections

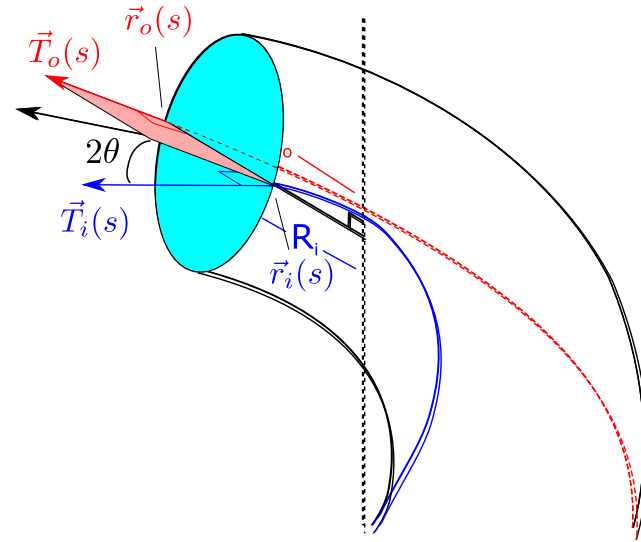
Tube diameter separates inner and outer helices:

$$D = R_o - R_i$$

Tangent vectors are offset by twice the actuator angle:

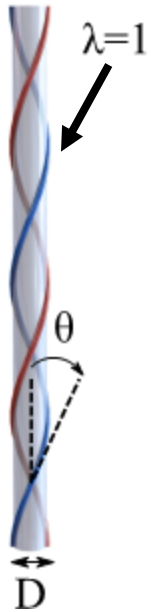
$$T_o(t) \cdot T_i(t) = \cos 2\theta$$

$$\cos 2\theta = \frac{b^2 + R_i R_o}{\sqrt{b^2 + R_i^2} \sqrt{b^2 + R_o^2}}$$



# General Actuator Kinematics

## Uniform Actuation Kinematics



Shape  $\rightarrow$  Actuator

$$D = R_o - R_i$$

$$\lambda = \frac{\sqrt{b^2 + R_i^2}}{\sqrt{b^2 + R_o^2}}$$

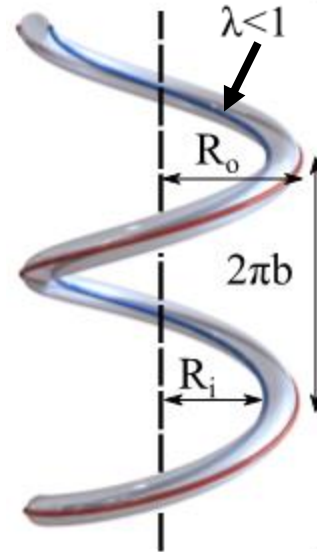
$$\theta = \frac{1}{2} \cos^{-1} \frac{b^2 + R_i R_o}{\sqrt{b^2 + R_i^2} \sqrt{b^2 + R_o^2}}$$

Actuator  $\rightarrow$  Shape

$$R_o = \frac{D(1 - \lambda \cos 2\theta)}{1 - 2\lambda \cos 2\theta + \lambda^2}$$

$$R_i = \frac{D\lambda(\cos 2\theta - \lambda)}{1 - 2\lambda \cos 2\theta + \lambda^2}$$

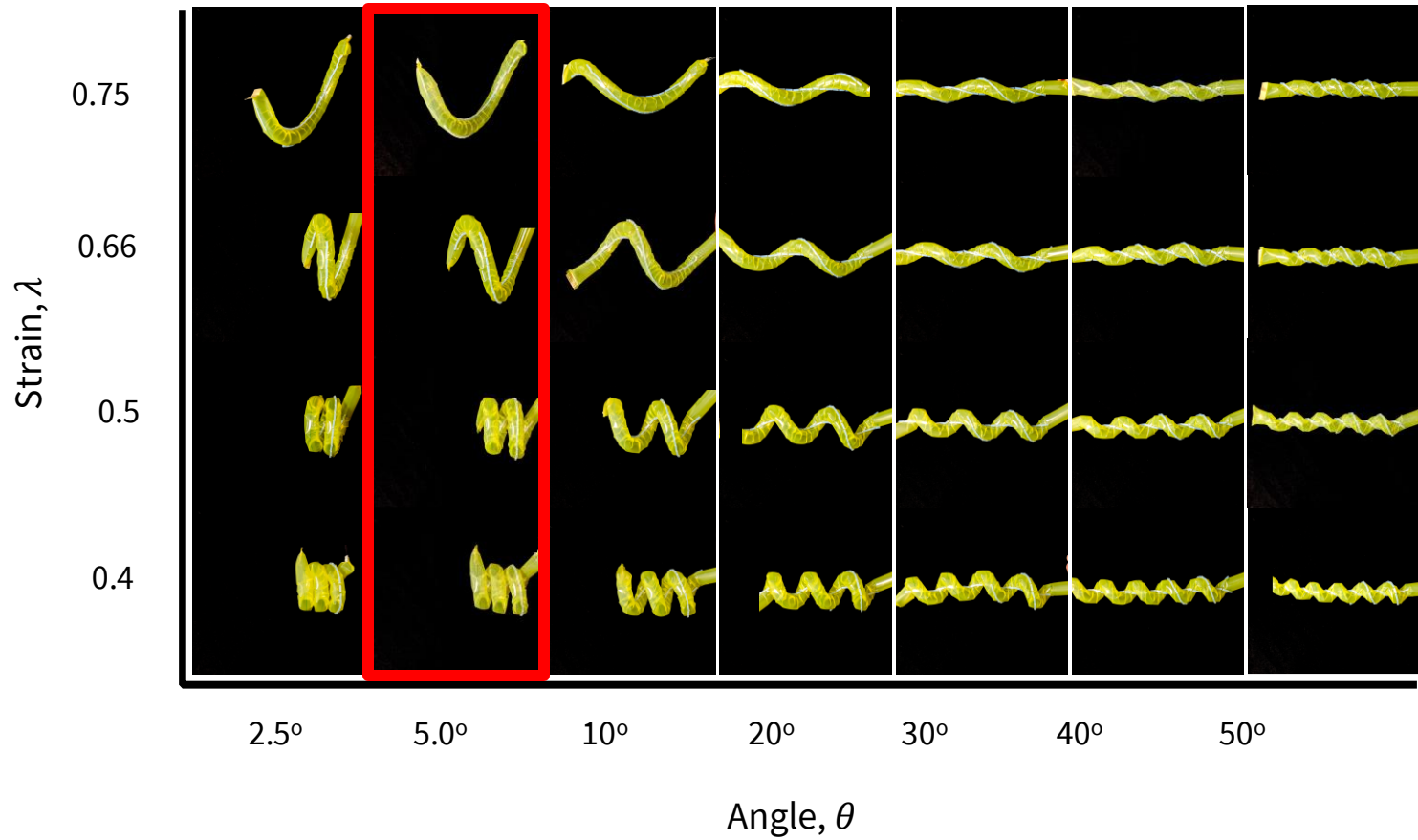
$$b = \frac{D\lambda \sin 2\theta}{1 - 2\lambda \cos 2\theta + \lambda^2}$$





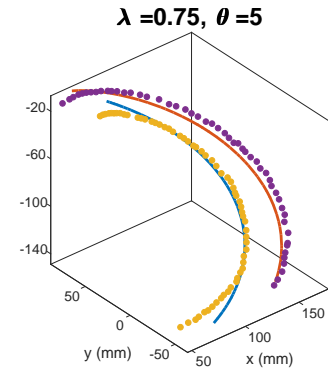
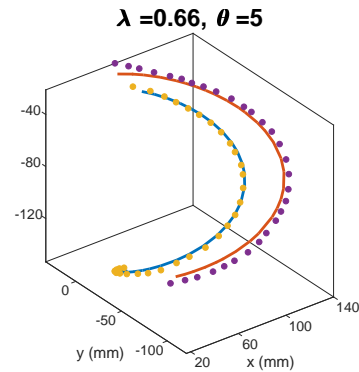
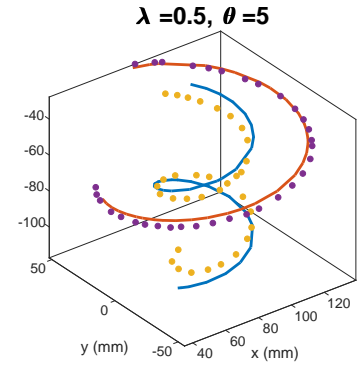
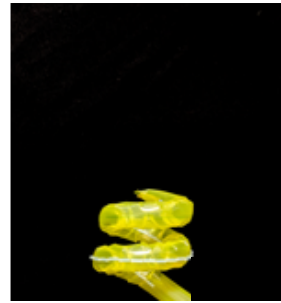
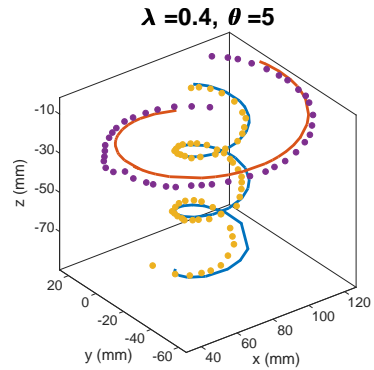
# General Actuator Kinematics

Model Validation: Helices



# General Actuator Kinematics

## Model Validation: Helices



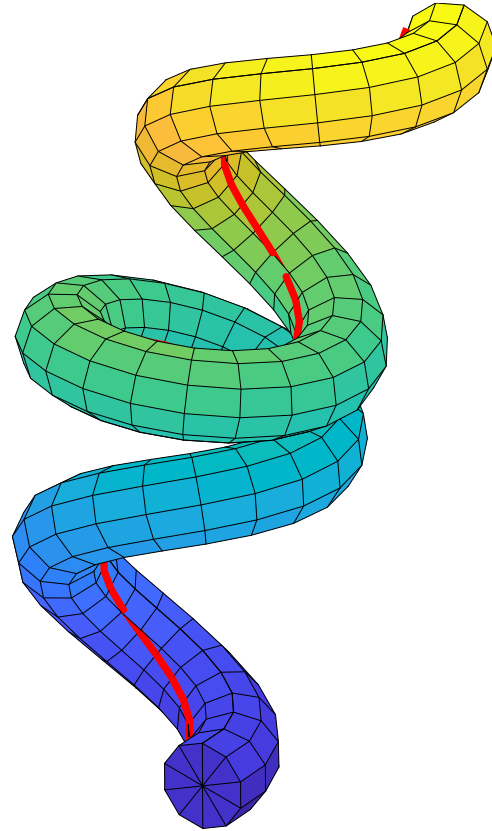
# General Actuator Kinematics

Generalizing Beyond Helices

$$\lambda = 0.5$$

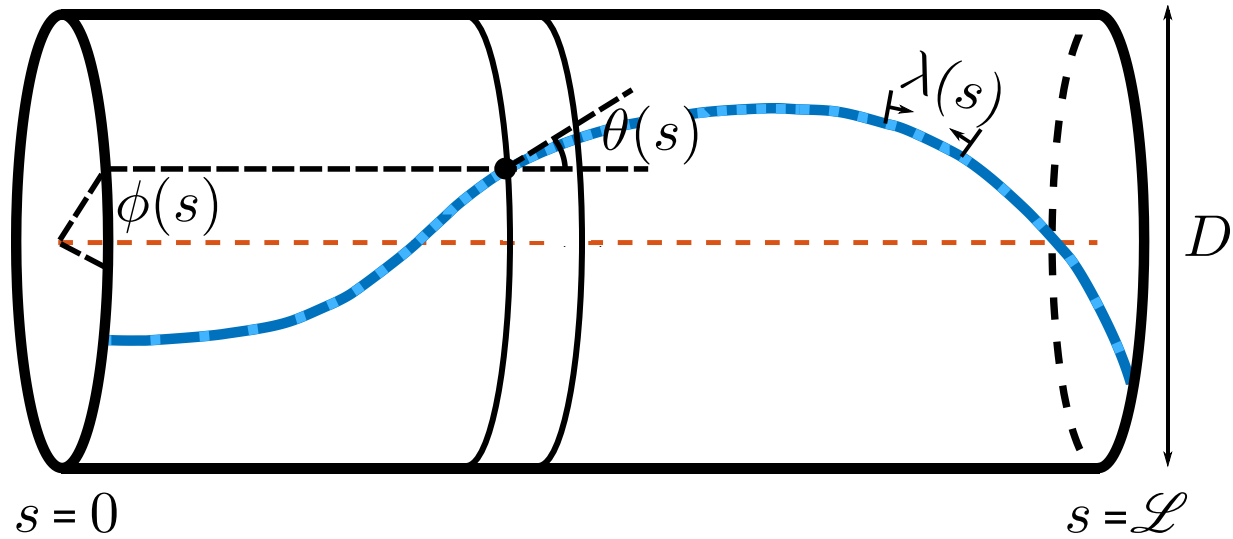
$$D = 0.5$$

$$\theta: 10^\circ \rightarrow 5^\circ \rightarrow 10^\circ$$



# General Actuator Kinematics

## Generalizing Beyond Helices



# General Actuator Kinematics

## Generalizing Beyond Helices

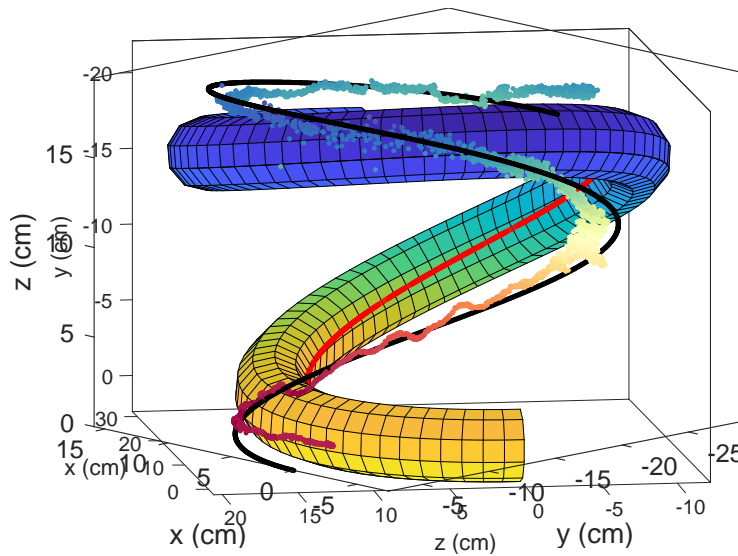
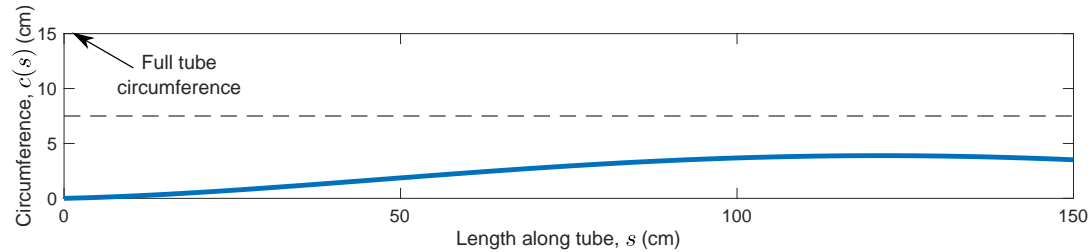
Transformation along a helical segment:

$$T_c(s) = \begin{bmatrix} \frac{R^2}{L^2} \cos \frac{\Delta \ell_\lambda}{L} + \frac{b^2}{L^2} & -\frac{R}{L} \sin \frac{\Delta \ell_\lambda}{L} & \frac{Rb}{L^2} \left(1 - \cos \frac{\Delta \ell_\lambda}{L}\right) & \frac{R^2}{L} \sin \frac{\Delta \ell_\lambda}{L} + \frac{b^2}{L} \frac{\Delta \ell_\lambda}{L} \\ \frac{R}{L} \sin \frac{\Delta \ell_\lambda}{L} & \cos \frac{\Delta \ell_\lambda}{L} & -\frac{b}{L} \sin \frac{\Delta \ell_\lambda}{L} & R \left(1 - \sin \frac{\Delta \ell_\lambda}{L}\right) \\ \frac{Rb}{L^2} \left(1 - \cos \frac{\Delta \ell_\lambda}{L}\right) & \frac{b}{L} \sin \frac{\Delta \ell_\lambda}{L} & \frac{b^2}{L^2} \cos \frac{\Delta \ell_\lambda}{L} + \frac{R^2}{L^2} & \frac{Rb}{L} \left(\frac{\Delta \ell_\lambda}{L} - \sin \frac{\Delta \ell_\lambda}{L}\right) \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

where  $L = \sqrt{R^2 + b^2}$  and  $\Delta \ell_\lambda = \Delta \ell \sqrt{\frac{\lambda^2 + 2\lambda \cos 2\theta + 1}{2(1 + \cos 2\theta)}}$  (along the centerline)

# General Actuator Kinematics

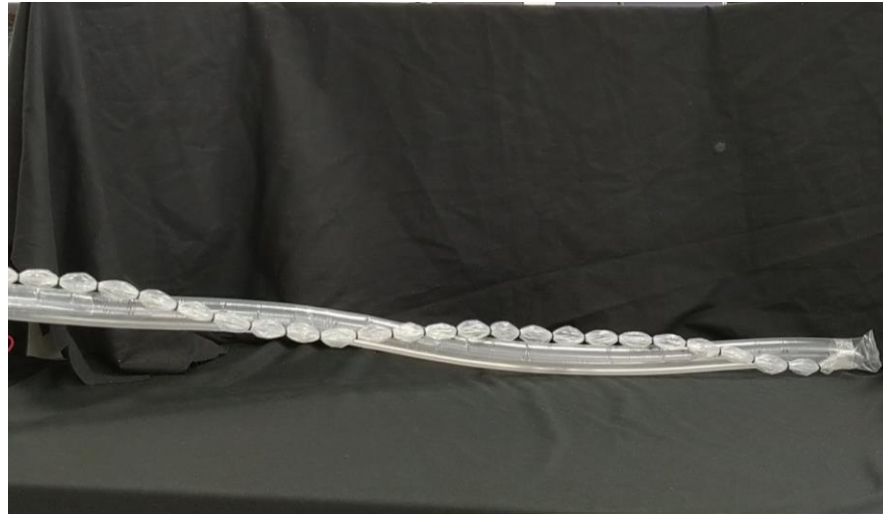
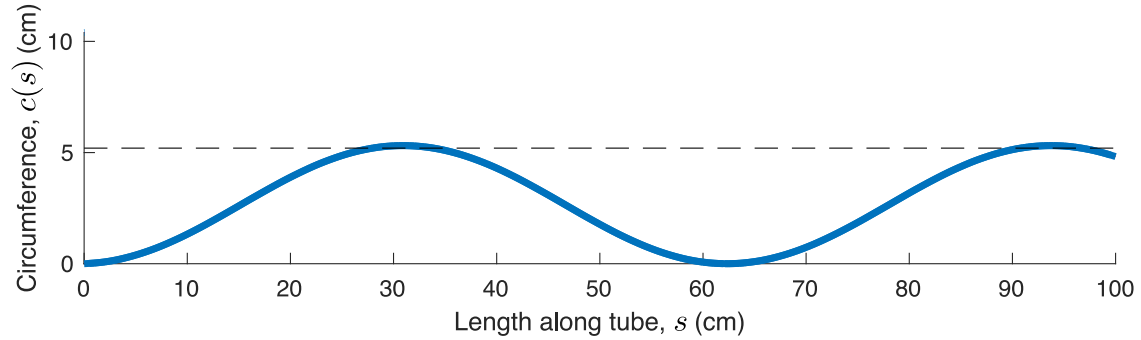
## Model Validation: Static Shapes



**RMSE = 0.45 cm**

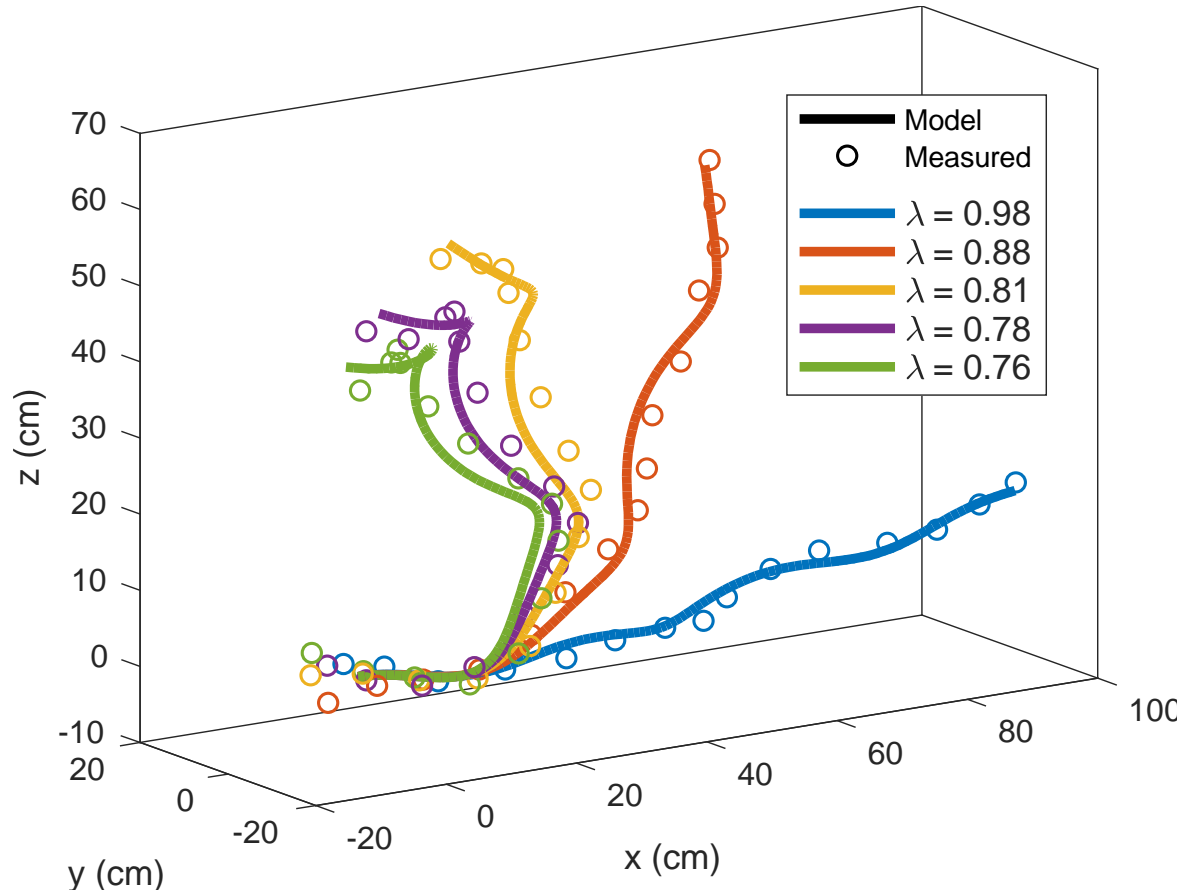
# General Actuator Kinematics

## Model Validation: Pneumatic Actuation



# General Actuator Kinematics

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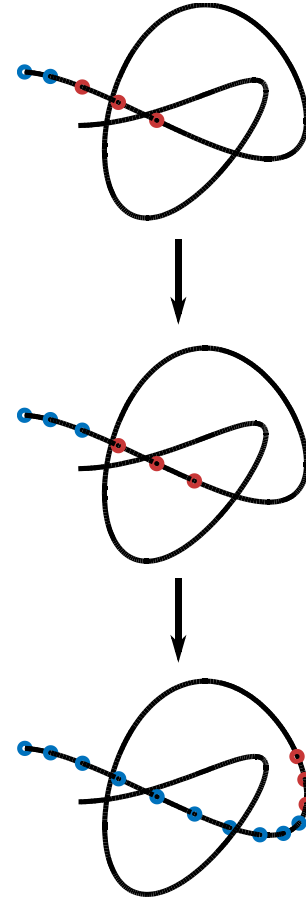




# General Actuator Kinematics

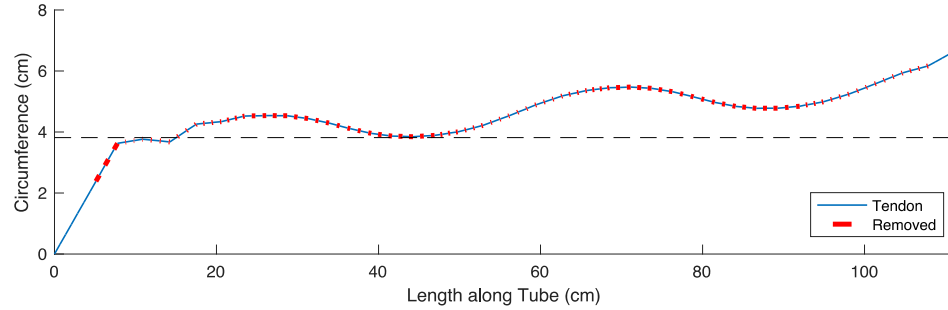
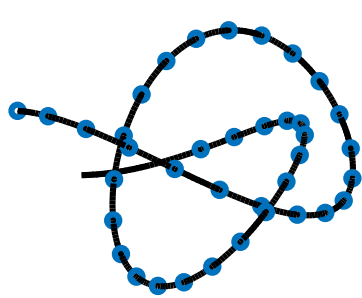
## Shape Matching Algorithm

- Find  $\theta, \lambda$  fit for each section of target shape to minimize error
- Consider the best fit for next  $n$  unfit sections
- Save the  $\theta, \lambda$  for the next segment only
- Repeat for length of target shape

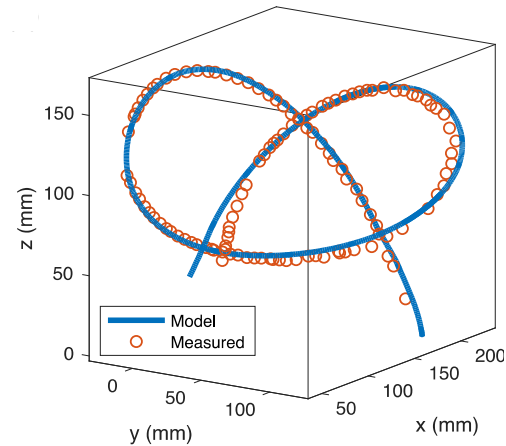


# General Actuator Kinematics

## Matching Desired Shapes



**RMSE = 6.88 mm**



# General Actuator Kinematics

## Growth and Actuation

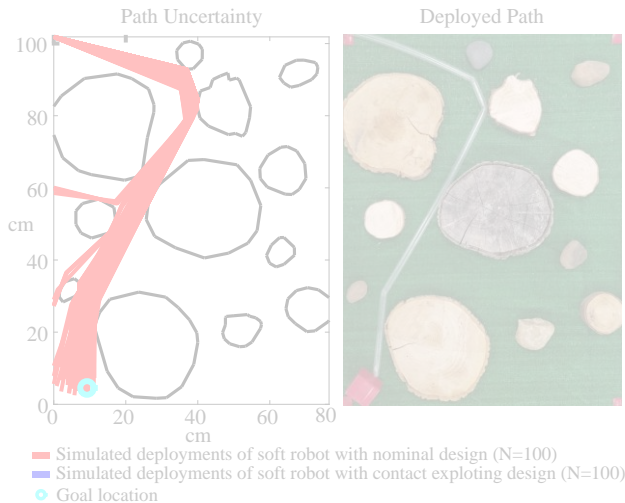
**During growth →**



**← After growth**

# Applying geometric constraints to simplify kinematic models

## Obstacle interaction to decrease uncertainty



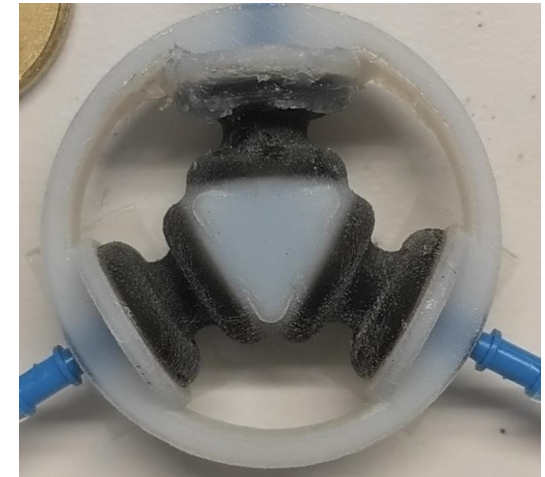
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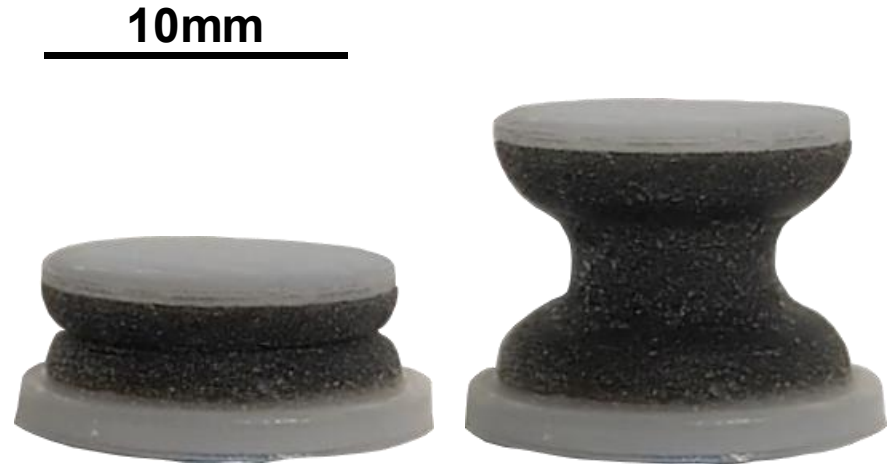
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## Component Actuator: Soft Bellows

Multi-material polyjet printing (Agilus and Digital ABS)

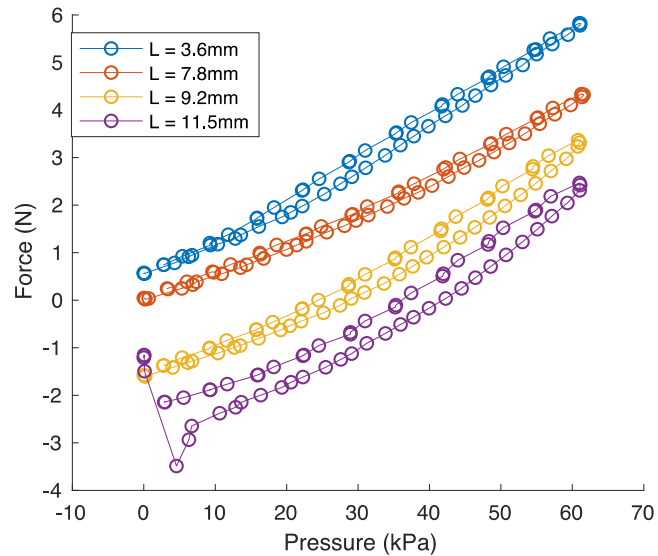
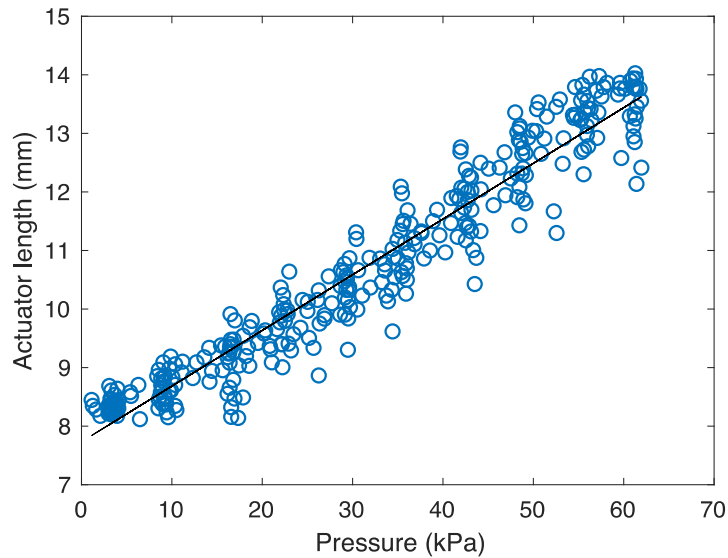
Change length through bending (and stretching) wall material

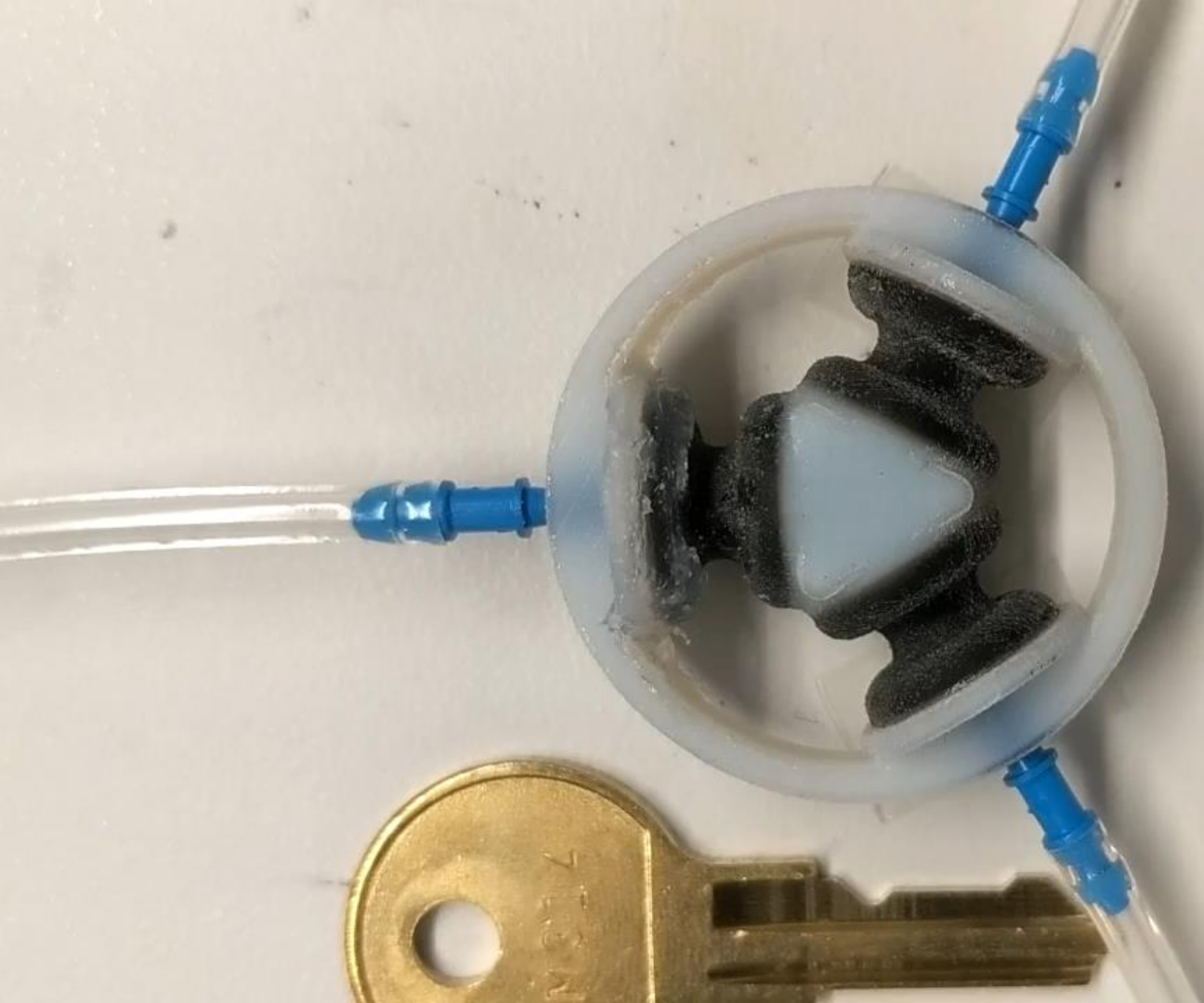
Total length change 340%





# Component Actuator: Soft Bellows





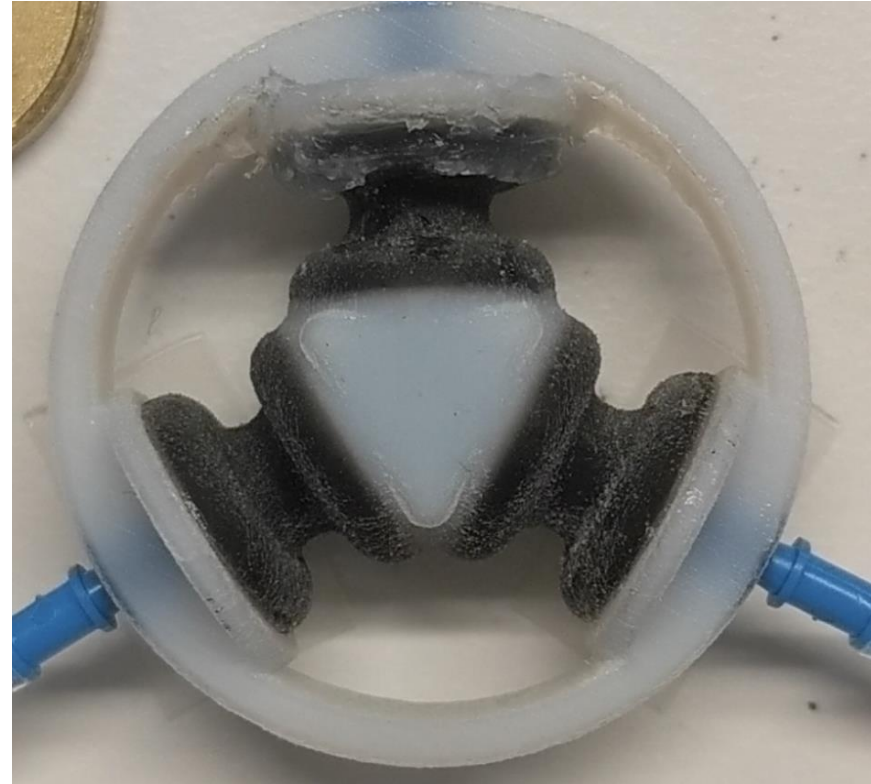


## Jacobian Model

$$\vec{F}_o = \mathbf{J} * \vec{P} = \sum_{i=1}^n P_i A_i \hat{u}_i$$

$$\mathbf{J} = A[\hat{u}_1 \hat{u}_2 \dots \hat{u}_n]$$

$$\hat{u}_i = \begin{bmatrix} \cos\left(\frac{2\pi}{n}(i-1) + \theta_o\right) \\ \sin\left(\frac{2\pi}{n}(i-1) + \theta_o\right) \end{bmatrix}$$



## Force Workspace

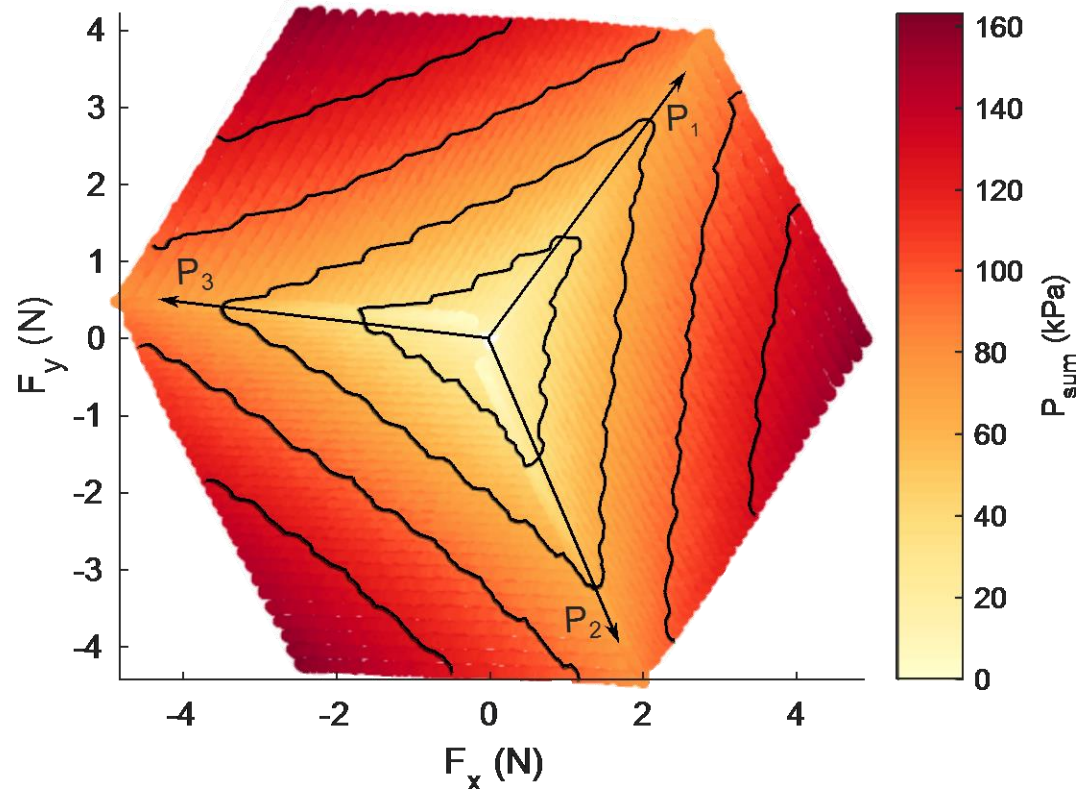
$$\vec{F}_o = \mathbf{J} * \vec{P} = \sum_{i=1}^n P_i A_i \hat{u}_i$$

$$\mathbf{J} = A[\hat{u}_1 \hat{u}_2 \dots \hat{u}_n];$$

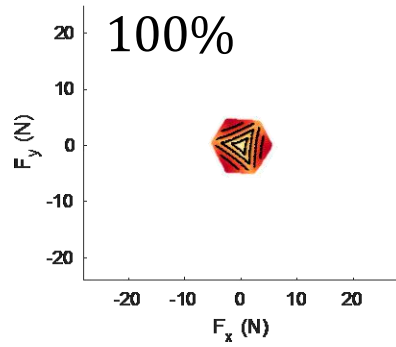
$$\hat{u}_i = \begin{bmatrix} \cos\left(\frac{2\pi}{n}(i-1) + \theta_o\right) \\ \sin\left(\frac{2\pi}{n}(i-1) + \theta_o\right) \end{bmatrix}$$

$$A = 54.4\text{mm}^2; \theta_o = -56^\circ$$

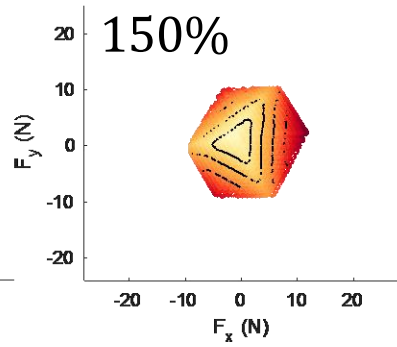
$$R^2 = 0.964$$



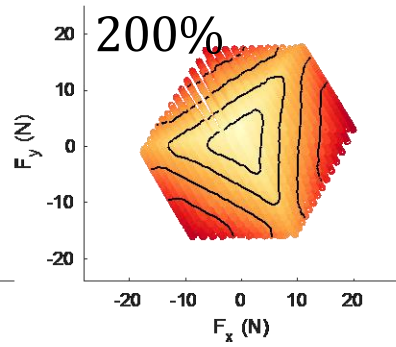
# Effect of Scaling



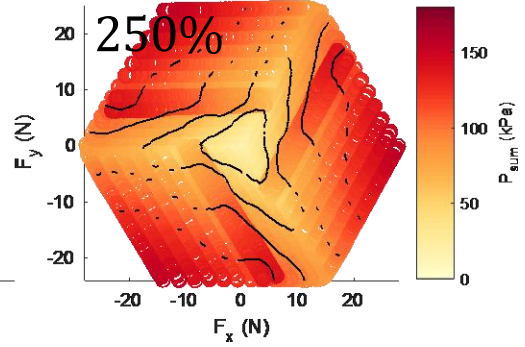
$A = 54.4 \text{ mm}^2$   
 $F_{max} = 4.9 \text{ N}$



$A = 126.3 \text{ mm}^2$   
 $F_{max} = 12.1 \text{ N}$   
155%

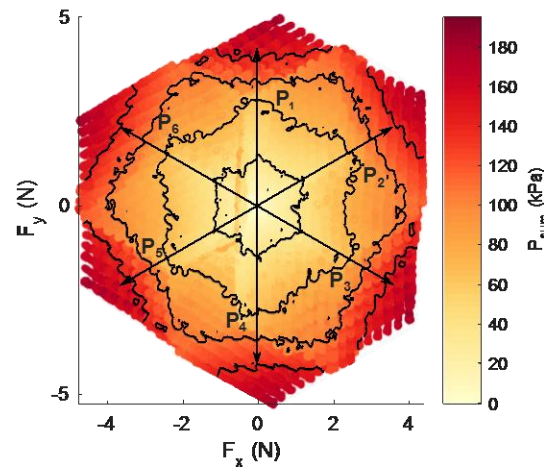
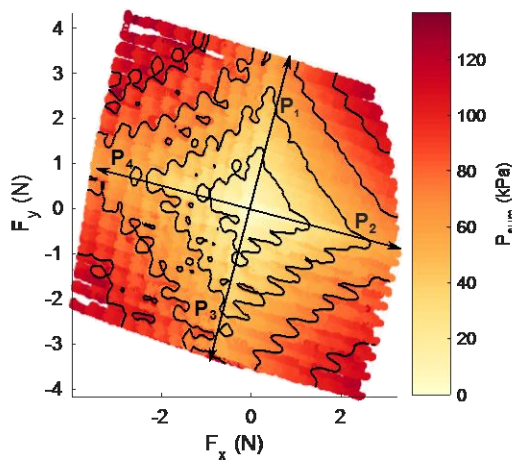
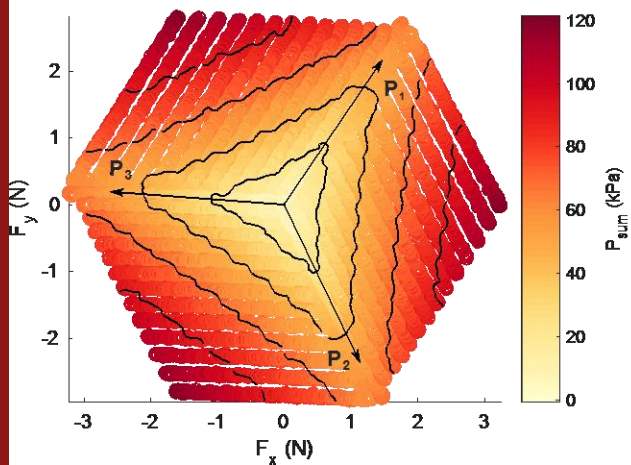


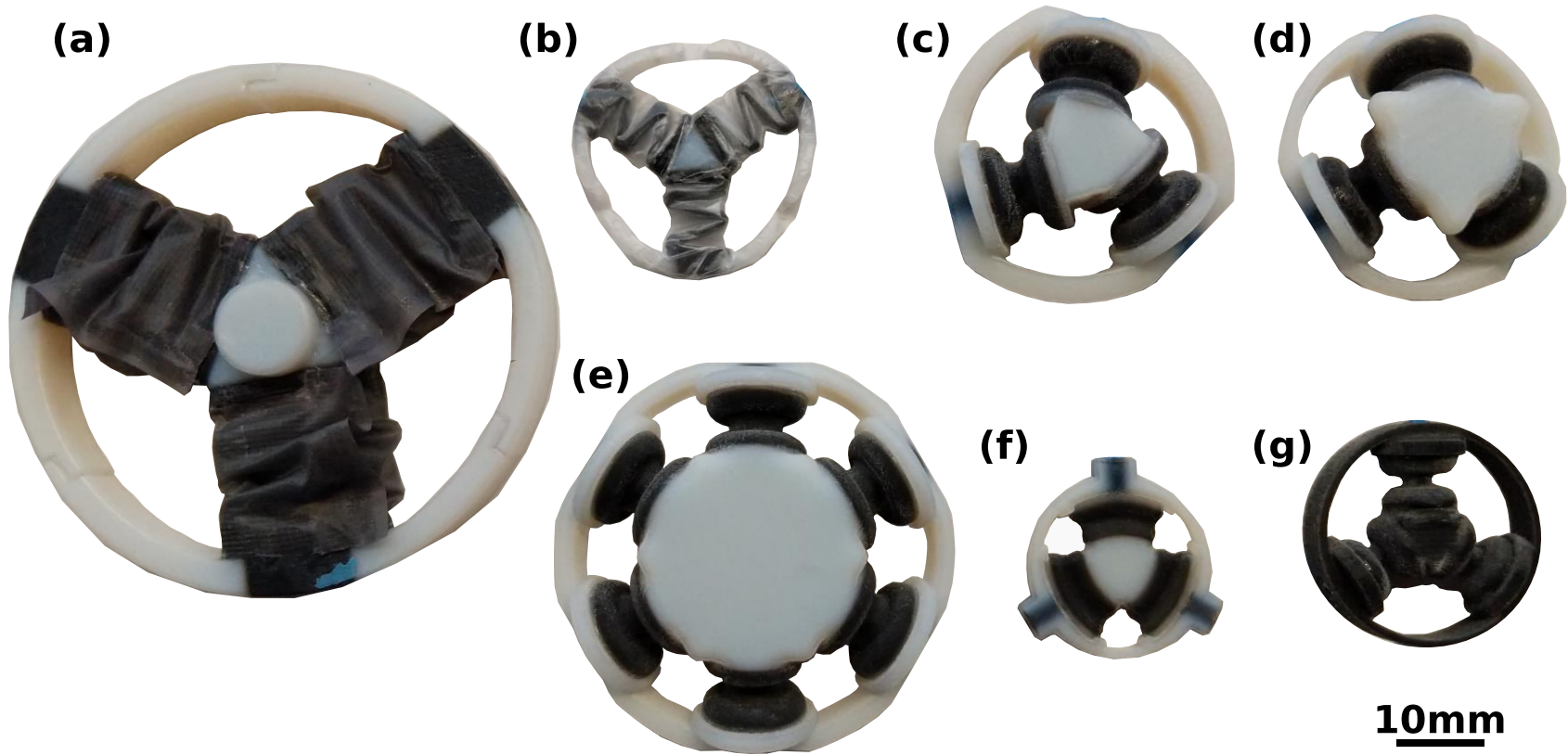
$A = 237.3 \text{ mm}^2$   
 $F_{max} = 20.8 \text{ N}$   
208%



$A = 305.4 \text{ mm}^2$   
 $F_{max} = 27.8 \text{ N}$   
238%

# Increasing Component Actuators

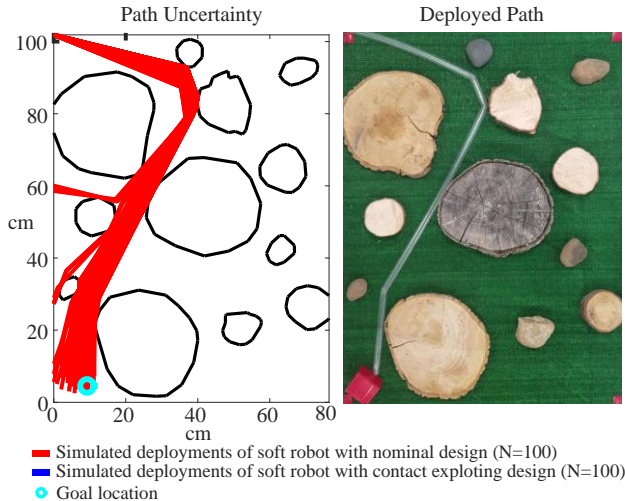






# Applying geometric constraints to simplify kinematic models

## Obstacle interaction to decrease uncertainty



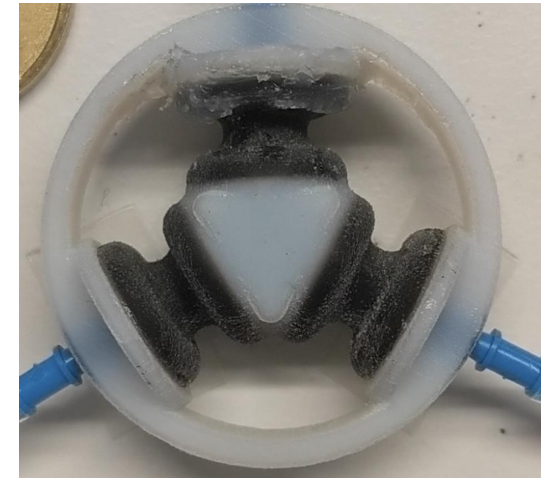
Greer, et al (2020). "Robust navigation of a soft growing robot by exploiting contact with the environment," *IJRR*.

## Geometric models of general actuation



Blumenschein, et al (2020). "Geometric Solutions for General Actuator Routing on Inflated-Beam Soft Growing Robots," *arXiv preprint arXiv:2006.06117*.

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Blumenschein, et al (2019) "Generalized Delta Mechanisms from Soft Actuators," *RoboSoft*.

## Conclusions

- Can develop building blocks for design and modeling through observation of heuristics, decomposition of complex designs, or targeted design.
- Created models predict behavior well enough to design more complex interactions
- The overall accuracy is limited by the assumptions and simplifications made when applying the geometric constraints
- In the future, applying methods like these can lead to more rapid prototyping and understanding of new soft robotic functions

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# Questions?

